Balance of microtubule stiffness and cortical tension determines the size of blood cells with marginal band across species

Serge Dmitrieff, Adolfo Alsina, Aastha Mathur, and François J. Nédélec

*Cell Biology and Biophysics Unit, European Molecular Biology Laboratory, 69117 Heidelberg, Germany

Edited by Timothy J. Mitchison, Harvard Medical School, Boston, MA, and approved February 14, 2017 (received for review November 1, 2016)

The fast bloodstream of animals is associated with large shear stresses. To withstand these conditions, blood cells have evolved a special morphology and a specific internal architecture to maintain their integrity over several weeks. For instance, nonmammalian red blood cells, mammalian erythroblasts, and platelets have a peripheral ring of microtubules, called the marginal band, that flattens the overall cell morphology by pushing on the cell cortex. In this work, we model how the shape of these cells stems from the balance between marginal band rigidity and cortical tension. We predict that the diameter of the cell scales with the total microtubule polymer and verify the predicted law across a wide range of species. Our analysis also shows that the combination of the marginal band rigidity and cortical tension increases the ability of the cell to withstand forces without deformation. Finally, we model the marginal band coiling that occurs during the disk-to-sphere transition observed, for instance, at the onset of blood platelet activation. We show that when cortical tension increases faster than cross-linkers can unbind, the marginal band will coil, whereas if the tension increases more slowly, the marginal band may shorten as microtubules slide relative to each other.

cytoskeleton | scaling | mechanics | blood platelet | theory

The shape of animal cells is determined by the cytoskeleton, including microtubules (MTs), contractile networks of actin filaments, intermediate filaments, and other mechanical elements. The 3D geometry of MTs in a multicellular organism is also largely determined by their adhesion to neighboring cells or to the extracellular matrix (1). This is, however, not the case for blood cells because they circulate freely within the fluid environment of the blood plasma. Red blood cells (RBCs) and thrombocytes in nonmammalian animals (2, 3), as well as platelets and erythroblasts in mammals (4, 5), adopt a simple ellipsoidal shape (Fig. 1A). This shape is determined by two components: a ring of MTs, called the marginal band (MB), and a protein cortex at the cell periphery.

In the case of platelets and nonmammalian RBCs, both components are relatively well characterized (Fig. 1). The cortex is a composite structure made of spectrin, actin, and intermediate filaments (Fig. 1B), and its complex architecture is likely to be dynamic (11–13). It is a thin network under tension (14), that on its own would lead to a spherical morphology (15). This effect is counterbalanced by the MB, a ring made of multiple dynamic MTs, held together by cross-linkers and molecular motors into a closed circular bundle (4, 16) (Fig. 1C). The MB is essential to maintain the flat morphology, and treatment with a MT-destabilizing agent causes platelets to round up (17). Platelets also respond to biochemical signals indicating a damage of the blood vessels, and during this activation, the MB is often seen to buckle (3). This phenomenon is reminiscent of the buckling of a closed elastic ring (18), but an important difference is that the MB is not a continuous structure of constant length.

Indeed, the MB is made of multiple dynamic MTs that are linked by MT-associated proteins. Because these connectors are not static, but instead bind and unbind, MTs could slide relative to one another, allowing the length of the MB to change. It was suggested in particular that molecular motors may drive the elongation of the MB (19), but this possibility remains mechanistically unclear. Moreover, the MB changes as MTs assemble and disassemble. However, in the absence of sliding, elongation or shortening of single MTs would principally affect the thickness of the MB (i.e., the number of MTs in the cross-section) rather than its length. These aspects have received little attention so far, and much remains to be done before we can understand how the original architecture of these cells is adapted to their unusual environment and to the mechanical constraints associated with it (7).

We argue here that, despite the potential complexity of the system, the equilibrium between MB elasticity and cortical tension can be understood in simple mechanical terms. We first predict that the main cell radius should scale with the total length of MT polymer and inversely with the cortical tension, and test the predicted relationship by using data from a wide range of species. We then simulate the shape changes observed during platelet activation (20), discussing that a rapid increase of tension leads to MB coiling, accompanied by a shortening of the ring, whereas a slow increase of tension leads to a shortening of the ring without coiling. Finally, by computing the buckling force of a ring confined within an ellipsoid, we find that the resistance of the cell to external forces is dramatically increased compared with the resistance of the ring alone.

Results

Cell Size Is Controlled by Total MT Polymer and Cortical Tension. We first apply scaling arguments to explore how cell shape is determined by the mechanical equilibrium between MB elasticity and cortical tension.

Significance

The discoidal shape of many blood cells is essential to their proper function within the organism. For blood platelets and other cells, this shape is maintained by the marginal band, which is a closed ring of filaments called microtubules. This ring is elastic and pushes on the cell cortex, a tense polymer scaffold associated with the plasma membrane. Dmitrieff et al. examined how the mechanical balance between these two components determine cell size, uncovering a scaling law that is observed in data collected from 25 species. The analysis also indicated that the cell can resist much higher mechanical challenges than the microtubule ring alone, in the same way as a tent with its cloth is stronger than the poles alone.

Author contributions: S.D. and F.J.N. designed research; S.D., A.A., and A.M. performed research; S.D. and A.A. analyzed data; and S.D., A.M., and F.J.N. wrote the paper.

The authors declare no conflict of interest.

This article is a PNAS Direct Submission.

This article contains supporting information online at www.pnas.org/lookup/suppl/doi:10.1073/pnas.1618041114/-/DCSupplemental.

1To whom correspondence should be addressed. Email: nedelec@embl.de.

This article contains supporting information online at www.pnas.org/lookup/suppl/doi:10.1073/pnas.1618041114/-/DCSupplemental.
and cortical tension. In their resting state, the cells are flat ellipsoids, and the MB is contained in a plane that is orthogonal to the minor cell axis. Assuming that the cell is discoid for simplicity \((R_1 = R_2 = R)\), the major radius \(R\) is also approximately the radius of the MB (Fig. 1D), and thus the MTs bundled together in the MB have a curvature \(C \sim 1/R\) and length of the ring is \(\sim 2\pi R\). Generically, the deformation energy of such a ring can be written \(E_r = 2\pi R^2\kappa r_1 = 2\pi\kappa r_1 / R\), in which \(\kappa r_1\) is the rigidity of the bundle, often written as \(YI\) (with \(Y\) the young modulus of the material and \(I\) its moment of inertia) (21). We first consider time scales larger than the dynamics of MT cross-linker binding and unbinding (approximately 10 s (22)), for which we can ignore the mechanical contribution of cross-linkers (10). In this limit, the MTs are mechanically independent, and we can assume \(\kappa r_1 = n\kappa\), with \(n\) the number of MTs in a cross-section of the ring and \(\kappa = 22\) pN \(\mu\)m \(^2\) the rigidity of an individual MT (23).

We can define \(L \approx 2\pi Rn\), which corresponds to the sum of the MTs’ lengths, and write the total elastic energy as \(E_B = \pi L^2 / R^2\). At time scales larger than a few seconds, the cortex can reorganize, and therefore we do not have to include contributions from its rigidity (24). Its effect can then be modeled by a surface energy associated with a surface tension \(\sigma\) (Fig. 1D). The surface area of a cell of thickness \(2\tau\) is \(S = 2\pi\tau^2[1 + O(\tau^2)]\), and if the cell is sufficiently flat, we can approximate the energy as \(E_T \approx 2\pi\sigma\tau^2\).

The equilibrium of the system corresponds to \(\partial_R(E_B + E_T) = 0\), leading finally to:

\[
R^4 = \frac{\kappa L}{4\pi\sigma}.
\]  

All other things constant, we thus expect \(R \propto L^{1/4}\). To verify this relationship, we used data from the literature (2), and for 25 species calculated \(L\) by multiplying the number of MTs in a cross-section by the length of the marginal band. The scaling is remarkably respected, over more than two orders of magnitude (Fig. 2A). By using Eq. 1, the fit provides an estimate of the cortical tension of \(\sigma \sim 0.1\) pN/\(\mu\)m, which is low compared with the tension \(\sigma \sim 100\) pN/\(\mu\)m of the actomyosin cortex of blebbing cell (25). However, RBCs have a cortex made of spectrin rather than actomyosin, and a much lower cortical tension is expected. Human RBCs, which are devoid of a marginal band, have a cortical tension of \(\approx 0.65\) pN/\(\mu\)m (26), because the spectrin cortex opposes the membrane tension (27) In contrast to this, we predict \(\sigma \approx 27\) pN/\(\mu\)m for human blood platelets, given that \(R \approx 1.6\) \(\mu\)m and \(L \approx 100\) \(\mu\)m (28), and this is close to the tension of blood granulocytes (35 pN/\(\mu\)m) (14).

The scaling observed across 25 species seems to confirm that, at long time scales, the mechanical balance between bending rigidity of the MTs and cortical tension define cell size (Fig. 1D). To verify the validity of this result for a ring made of multiple dynamically cross-linked MTs, we developed a numerical model.
in Cytosim, a cytoskeleton simulation engine (29). Cytosim solves the Langevin equation ($\text{viscosity} \times \text{velocity} = \text{forces} + \text{Brownian noise}$), describing the motion of bendable filaments that are discretized into model points. The forces stem from the rigidity of the filaments (tending to minimize bending energy), links between filaments (modeled as Hookean springs between filaments), and confinement within the cell. The Brownian noise is a stochastic force calibrated from temperature. For this work, we extended Cytosim to be able to model a contractile surface under tension that can be deformed by the MTs. The cell shape is restricted to remain ellipsoidal and is described by six parameters: the lengths of three axes $R_1$, $R_2$, and $r$ and a rotation matrix (i.e., three angles describing the cell orientation in the space). Because RBCs have active mechanisms to maintain their volume (30), we also constrained the three lengths to keep the volume of the ellipsoid constant. To implement confinement, any MT model point located outside the cell is subject to inward-directed force $f = k \delta$, in which $\delta$ is the shortest vector between the point and the surface and $k$ the confining stiffness. Here, for each force $f$ applied on a MT, an opposite force $-f$ is applied to the surface, in agreement with Newton’s third law. The rates of change of the ellipsoid parameters are then given by the net force on each axis, divided by $\mu$, an effective viscosity parameter (SI Text, section 1.3 and Fig. S1). The value of $\mu$ affects the rate at which the cell shape can change, but not the shape that will eventually be reached. This approach is much simpler than using a tessellated surface to represent the cell, and still general enough to capture the shape of blood platelets (3, 6) and several RBCs (8, 31) (Fig. 2).

To model resting platelets, we simulated marginal bands made of 10–20 MTs of fixed length 9–16 µm (4) with 0 or 10,000 cross-linkers, confined in a cell of volume 8.4 µm$^3$ with a tension $\sigma = 0.45–45$ pN/µm. Initially the filaments had random orientations, and we simulated the system for $> 6$ min, which was enough time for them to align at the periphery and balance the cortical tension given the viscosity. This also allowed for multiple rounds of cross-linker binding/unbinding events. We found that the numerical results agree with the scaling law over a very large range of parameter values, as illustrated in Fig. 2B. Interestingly, simulated cells were slightly larger than predicted analytically. This is because MTs of finite length do not exactly follow the best fit radius, and their ends are less curved, thus exerting more force on the cell. This means that the value of the tension computed from the biological data (σ $\sim$ 0.1 pN/µm) is slightly underestimated. More importantly, a simulated cell has the same size at equilibrium with or without cross-links (compare black and gray dots on Fig. 2B). This shows that, if they are given time to freely reorganize, cross-linkers do not affect the mechanical equilibrium of the system. To understand the response of the system that occurs at short time scale, it is, however, necessary to consider the cross-linkers.

**The MB Behaves Like a Viscoelastic System.** During activation, mammalian platelets round up before spreading, and within a few seconds, their MB coils (19). A similar response is seen also in thrombocytes (3). This process can be triggered by several activators, including thrombin and ADP, that bind to G-protein-coupled receptors (32) and activate several downstream events. Among them, RhoA may induce actin contraction (33), possibly through its role in myosin light-chain phosphorylation (34). To observe platelet activation experimentally, we extracted mice platelets and exposed them to ADP, causing an often-reversible activation. By monitoring the MB with SiRTubulin, a bright docetaxel-based MT dye, we could record the MB coiling live, Fig. 3A (SI Text, section 4). The MB coils according to the baseball-seam curve, which is the shape that an incompressible elastic ring would adopt when constrained into a sphere smaller than its natural radius (35). Thus, at short time scale, the MB seems to behave as an incompressible ring, and we reasoned that this must be because cross-linkers prevent MTs from sliding relative to each other. To analyze this process further, we returned to Cytosim. After an initialization time, in which the MB assembles as a ring of MTs connected by cross-linkers, cortical tension is increased stepwise. The cell as a consequence becomes nearly spherical, and, because we assumed that the volume should be constant, the radius of this sphere was smaller than the largest radius that the cell had at low tension. As a result, the MB adopted a baseball-seam shape (Fig. 3B). Over a longer period, however, the MB regained a flat shape, as MTs rearranged into a new, smaller ring (Fig. 3A). In conclusion, the simulated MB is viscoelastic (Fig. 3B). At short time scales, MTs do not have time to slide, and the MB behaves as an incompressible elastic ring. At long time scales, the MB behaves as if cross-linkers were not present, with an overall elastic energy that is the sum of individual MT energies. Thus, overall, the ring behavior seems to transition from purely elastic at short time scales, to viscoelastic Kelvin–Voigt law at long time scales (Fig. 3C). The transition between the two regimes is determined by the time scale at which cross-linkers permit MTs to slide.

**The Cell Is Unexpectedly Robust.** The MB in blood cells is necessary to establish a flat morphology, but also to maintain this morphology in the face of transient mechanical challenges, for example as the cell passes through a narrow capillary (7). We thus investigated how the cortex effectively reinforces the
MB, making the cell a stronger object than the MB alone. Specifically, we calculated the resistance of the cell to deformations that would require its marginal band to coil, on a short time scale, during which cross-linkers do not reorganize. We therefore considered the MB as a closed ring of constant length $L$ and uniform rigidity $\kappa_c$. We first examined the mechanics of this ring within a sphere and then extended these results to a nondeformable ellipsoid. The shape of a ring in a sphere was previously calculated numerically (35), and we extended this result by deriving analytically the force $f_B$ required to buckle a confined ring (SI Text, section 1.2.2 and Fig. S2). If $E_B$ is the energy of a buckled MB, the force is:

$$f_B = -\lim_{L \to 2\pi R} \frac{\partial E_B}{\partial \kappa_c} = 8\pi \frac{\kappa_c}{R^2}. \quad [2]$$

We verified this relation in simulations, with $L = 2\pi R(1 + \epsilon)$, where $\epsilon > 0$, which made the ring slightly oversized compared with its confinement. Given the confining stiffness $k$, the force applied to each model point of the ring is $k\epsilon$. If $n$ is the number of model-points in the rings (i.e., $n = L/s$ where $s$ is the discretization parameter of the ring), the total centripetal force is $nk\epsilon$. Hence, we expected the ring would buckle if $k$ exceeds $k_c = \frac{1}{8\pi}\frac{E_B}{R^2}$. Upon systematically varying $k$ in the simulation (Methods), we indeed found that the ring coils for $k > k_c$ (Fig. 4A). We next simulated oblate ellipsoidal cells, with $R_1 = R_2 = R$ and $r < R$, and we varied the flatness of the cell by changing $r/R$. We found that the measured critical confinement $k^*$ is indeed $k_c$, for $r = R$, but increases strongly with $1 - r/R$ (Fig. 4A and B). We also found that the mode of deformation increases with the cell flatness (Fig. 4A, shades of red). This is because, as the cell gets flatter, larger deformations along the short axis are increasingly penalized, and higher modes of deformation (such as the chair shape; Fig. 4C, c) become more favorable than the baseball-seam curve (Fig. 4C, d), because the magnitude of their out-of-plane deviations is smaller. This increase of the critical buckling force with cell flatness implies that an uncoiled marginal band in a flat cell could be metastable.

Platelets and nonmammalian RBCs have an isotropy ratio $r/R \approx 0.25$ (Fig. 4C, c), which makes them $>10$ times more resilient than a spherical cell with similar characteristics. Direct micropipette aspiration showed that destabilizing MTs or actin lead in both cases to an increased deformability, confirming that actin and MT systems determine the rigidity of the cell together (36).

**Coiling Stems from Cortical Tension Overcoming MB Rigidity.** We then considered the case of a ring inside a deformable ellipsoid of constant volume $V_0 = \frac{4}{3}\pi R_0^3$, governed by a surface tension $\sigma$. The length of the ring $L$ is set with $L > 2\pi R_0$, such that we expected the ring to remain flat at low tension and to be coiled at high tension, because it does not fit in the sphere of radius $R_0$. In simulations, starting from a flat ring, we observed as predicted the existence of a critical tension $\sigma^*_c$, above which the ring is buckled (Fig. 5A). This shows that increasing $\sigma R_0^2/\kappa_c$ (i.e., increasing the ratio of cortical tension over ring rigidity) leads to cell rounding. Thus, either increasing the cortical tension or weakening the ring lead to coiling. Starting from a buckled ring, decreasing the tension below a critical tension $\sigma^*_c$ also leads to the cell flattening, as predicted. However, our simulations showed that $\sigma^*_c < \sigma_f$, and thus for $\sigma^*_c < \sigma < \sigma_f$, a cell initially flat remains flat, whereas a cell initially round remains round (Fig. 5). Hysteresis is the hallmark of bistability, and we had predicted this bistability in the previous section by showing that the flat configuration is metastable. This metastability (i.e., the fact that a MB in a flat cell has a higher buckling threshold than in a spherical cell) allows the cell to withstand very large mechanical constraints such as shear stresses. A platelet typically has $L/R_0 \approx 10$ (i.e., an isotropy $r/R \approx 0.25$) and is therefore in the region where the flat MB is extremely metastable. In this regime, extending the MB does not cause buckling, but increasing the tension does.

**Discussion**

We have examined how MB elasticity and cortical tension determine the morphology of blood cells. Equilibrium between these forces predicts a scaling law, $4\pi R^4 = \kappa L/\sigma$, in which $L$ is the sum of the lengths of the MTs inside the cell, $\kappa$ is the bending rigidity of MTs, and $\sigma$ is the cortical tension. Remarkably, values of $R$ and $L$ measured for 25 species conform to this scaling law. We caution that these observations were made for nondiscoidal RBCs (where the two major axes differ), indicating that other factors not considered here must be at work (7). In human RBCs, perturbation of the spectrin meshwork can lead to elliptical RBCs (37), suggesting that the cortex can impose anisotropic tensions, whereas another study suggests that MB-associated actin can sequester the MB into an elliptical shape (38). Cortical anisotropy would be an exciting topic for future studies, but this may not be needed to understand wild-type mammalian platelets.
Finally, calculating the buckling force of a cell containing an elastic ring and a contractile cortex led to a surprising result. We found that the buckling force increased exponentially with the cell flatness, because the cortex reinforces the ring laterally. This makes the MB a particularly efficient system to maintain the structural integrity of blood cells. For transient mechanical constraints, the MB behaves elastically, and the flat shape is metastable, allowing the cell to overcome large forces without deformation. However, as we observed, the viscoelasticity of the MB allows the cell to adapt its shape when constraints are applied over long time scales, exceeding the time necessary for MB remodeling by cross-linker binding and unbinding. It will thus be particularly interesting to compare the time scale at which blood cells experience mechanical stimulations in vivo with the time scale determined by the dynamics of the MT cross-linkers.

Methods

Simulations. MTs of persistence length $l_p$ are described as bendable filaments of rigidity $\kappa = k_B T / l_p$, in which $k_B T$ is the thermal energy. The associated bending energy is $\frac{1}{2} \kappa \int (\partial^2 r / \partial s^2)^2 ds$, where $r(s)$ is the position as a function of the arclength $s$ along the filament. The dynamics of such a system was simulated in Cytosim, an Open Source simulation software (29). In Cytosim, a filament is represented by model points distributed regularly defining segments of length $s$. Fibers are confined inside a convex region of space $\Omega$ by adding a force to every model point that is outside $\Omega$. The force is $f = k \mathbf{p} (\mathbf{r} - \mathbf{r}_0)$, where $\mathbf{p}$ is the projection of the model point $\mathbf{r}$ on the edge of $\Omega$, and $k$ is a stiffness constant. For this work, we implemented a deformable elliptical surface confining the MTs, parameterized by six parameters. The evolution of these parameters is implemented using an effective viscosity (SI Text, section 1.3). To verify the accuracy of our approach, we first simulated a straight elastic filament, which would buckle when submitted to a force exceeding $\frac{\pi}{4} \kappa C / l^2$, as shown by Euler. Cytosim recovered this result numerically. We then calculated the critical tension necessary for the buckling of MTs in a prolate ellipsoid. The simulated critical tension corresponds very precisely to the theoretical prediction (43) (SI Text, section 1.4 and Fig. S1).

To calculate the cell radius as a function of $\kappa / \sigma$, we used a volume of $8 \times 10^3 \mu m^3$ (close to the volume of a platelet), with a tension $\sigma \sim 0.45$ to 45 pN/μm, consistent with physiological values. We simulated 10 – 20 MTs with a rigidity 22 pNμm² as measured experimentally (23). MTs have lengths in 9 – 16 μm and are finely represented with a segmentation of 125nm. The cross-linkers have a resting length of 40 nm, a stiffness of 91 pN/μm, a binding rate of 10 s⁻¹, a binding range of 10 nm, and an unbinding rate of 6 s⁻¹. An example of simulation configuration file is provided in SI Text, section 2. When considering an incompressible elastic ring, we used a cell of volume $4 / 3 \pi R_0^3$, where $R_0$ is the radius of the spherical cell. For simplicity, we can renormalize all lengths by $R_0$ and thus all energies by $\kappa / R_0$, where $\kappa$ is the ring rigidity. We simulate a cell with a tension $\sigma = 5 – 18 \kappa / R_0^3$, and a ring of length $1 – 6 \times 2 \pi R_0$. To test the effect of confinement, we place an elastic ring of rigidity $\kappa$, in an ellipsoid space of principal radii $R, R, R$ in which $r < 1$. The elastic ring has a length $(1 + 1/2)2\pi R$, in which $\epsilon = 0.05$. An extensive list of parameters and their values are given in SI Text, section 1.2. To estimate the coiling level of a MB, we first perform a principal component analysis using all of the MT’s model points. The coordinate system is then rotated to bring the vector $\mathbf{u}_0$ in the direction of the smallest eigenvalue. We then define the degree of coiling as the deviation in $Z$ divided by the deviations in $XY$: $C = \sqrt{\sum Z^2 / \sum X^2 + \sum Y^2}$. Thus, $C$ is independent of the size of the cell and only measures the deformation of the MB.

To measure the critical value of a parameter $\theta$ (e.g., tension or confinement) leading to coiling, we computed the derivative of the degree of coiling $C$, with respect to this parameter. Because buckling is analogous to a first-order transition, the critical value $\theta^*$ can be defined by: $\partial C / \partial \theta|_{\theta=\theta^*} = -\max (|\partial C / \partial \theta|)$. We calculated the Fourier modes of deformation by transforming the $z$-coordinates of the MT model points.

Acknowledgments. Thank S. Correia for technical assistance; A. Diz-munoz, R. Prevedel, and N. Minc for critical reading; and European Molecular Biology Laboratory (EMBL) IT support for performance computing. This work was supported by the EMBL and the Center for Modeling in the Biosciences (S.D.).


Supporting Information

Dmitrieff et al. 10.1073/pnas.1618041114

SI Text

1. Simulation of MTs/Cortex Interaction

To understand cell shape maintenance, one needs to model the interaction between the cellular cortex and the MB. The structure of the MB is well known, compared with the organization of the cortex, which is less well characterized. We thus decided to represent the MTs individually, and the cortex effectively as a continuous deformable surface. Treating the interactions between a discretized (e.g., triangulated) surface and discrete filaments can be demanding computationally, because such a surface would have a very large number of degrees of freedom. In contrast, we describe here how the problem remains relatively simple for a continuous shape that is defined by a small set of parameters.

1.1. General Formulation.

1.1.1. Forces and parameterization. Let \( S(\{p_k\}) \) be a surface defined by \( n \) parameters \( \{p_k\}_{k=1}^n \). Let \( \{f_i\}_{i=1}^m \) be the set of forces applied on \( S \) at the points \( \{r_i\}_{i=1}^m \). Assuming forces to be conservative, they are defined as \( -f_i = \partial E / \partial r_i \), where \( E \) is the energy of the system (excluding the surface). One can define “effective forces” \( \{\phi^k\}_{k=1}^n \) associated with each degree of freedom of the surface:

\[
\phi^k = -\frac{\partial E}{\partial p_k} = \sum_{i=1}^m f_i \frac{\partial r_i}{\partial p_k}.
\]

We can define \( \delta E \) the infinitesimal change in energy after an infinitesimal set of displacements \( \delta r_i \), and then compute it as a function of the infinitesimal set of parameter changes \( \delta p_k \).

\[
\delta E = - \sum_{i} \delta r_i \cdot f_i. \tag{S2}
\]

\[
\delta r_i = \sum_k \delta p_k \frac{\partial r_i}{\partial p_k}. \tag{S3}
\]

\[
\delta E = - \sum_k \delta p_k \phi^k. \tag{S4}
\]

To write Eq. S3, we had to assume that any displacement of the surface (allowed by the constraints) can be described in terms of \( p_k \), i.e., that \( S(\{p_k\}) \) is surjective. It is interesting here to note that \( \phi^k \) has the dimension of a force if \( p_k \) is a length, whereas it has the dimension of a torque (i.e., an energy) if \( p_k \) is an angle.

1.1.2. Constraints. In many cases, constraints can be added by modifying the energy functional following the method of Lagrange. For instance, to maintain the volume constant, we define an energy \( E' = E + PV \), where \( V \) is the volume and \( P \) is the pressure; here \( P \) is also a Lagrange multiplier, and we have to calculate its value appropriately to obtain \( V = V_0 \). The pseudoforces \( \phi^k \) associated to pressure are:

\[
\phi^k_P = -P \frac{\partial V}{\partial p_k}. \tag{S5}
\]

1.2. Deformable Ellipsoid.

In this section, we describe a surface in 3D. We model an ellipsoid centered around the origin, with a fixed volume \( V_0 \) and a surface tension \( \sigma \), which is an associated energy \( E_0 = \sigma S \), if \( S \) is the surface area of the ellipsoid. The ellipsoid is described by its principal directions \( u_{1,2,3} \) and their length (i.e., the radii of the ellipse) \( a_{1,2,3} \). We will also use the orientation matrix \( U = [u_1, u_2, u_3] \). By construction, \( U \) is a rotation matrix of determinant 1. In the simulation, this rotation matrix describes the orientation of the ellipse in space and does not apply to filaments within. This matrix is thus more appropriately seen as the inverse rotation that applies to all of the filaments, with respect to the cell envelope that confines them. The orientation in space of the ellipsoid (cell) is not relevant for this study, which is solely concerned with cell shape.

1.2.1. Surface tension. We can compute the pseudoforces associated to surface tension as:

\[
\phi^k_\sigma = -\sigma \frac{\partial S}{\partial a_k}. \tag{S6}
\]

The surface area of an ellipsoid is a complex special function that is not a combination of the usual functions. For convenience, we used an analytical approximation of the area:

\[
S(a_1, a_2, a_3) \approx 4\pi \frac{(a_1 a_2)^{\frac{2}{3}} + (a_2 a_3)^{\frac{2}{3}} + (a_3 a_1)^{\frac{2}{3}}}{3}, \tag{S7}
\]

for which \( p = 1.6075 \) is an empirical parameter. This formula yields an error usually below a percent.

1.2.2. Point forces. To add the contribution of the external forces exerted by the MTs on the surface, we need to determine \( \partial r/\partial p_k \). The position of a point on the surface of the ellipsoid is defined by two angles \( \theta, \phi \) as:

\[
r = u_1 a_1 \cos \theta \sin \phi + u_2 a_2 \sin \theta \sin \phi + u_3 a_3 \cos \phi. \tag{S8}
\]

Therefore, we have:

\[
\frac{\partial r}{\partial a_k} = \frac{r \cdot u_k}{a_k}. \tag{S9}
\]

Because we assumed that the boundaries offer no friction, all forces are normal to the surface. The contribution \( \phi^k_{ang} \) of a force \( f \) at a point \( r \) of the surface is:

\[
\phi^k_{ang} = f \cdot u_k \frac{r \cdot u_k}{a_k}. \tag{S10}
\]

We can now compute the torque generated by \( f \). In 2D, it would be convenient to describe the ellipse orientation by an angle \( \theta \), and the result is that the “angular force” \( \phi^k_\theta \) is the torque \( r \times f \). We will assume that this is general and stays true in 3D; thus, we can write \( \phi^k_{ang} \) directly as a vector:

\[
\phi^k_{ang} = r \times f. \tag{S11}
\]

1.2.3. Volume conservation. To implement volume conservation, we need to find a pressure \( P \) such that \( (V - V_0)/V_0 < \epsilon \), where \( \epsilon \) is a (small) tolerance parameter. We used Newton’s method to find a zero of \( (V - V_0)/V_0 \) and reach the desired aim for \( V \). This method works very well if \( V(P) \) is monotonous, which is always the case here.

The volume of the ellipse is \( V = \frac{4}{3} \pi a_1 a_2 a_3 \), and, therefore, using the Lagrange multiplier \( P \) to conserve the volume, we can write:
\[ \phi_p^b = \frac{4}{3} \pi^b \frac{a_1 a_2 a_3}{a_c}. \]  

**1.3. Time Evolution.** We can now define the time evolution of the ellipse. We assume a unique viscosity \( \mu \) associated to the change of size of the ellipse and a rotational viscosity \( \mu_{\alpha\beta} \).

\[ \dot{a}_k = \frac{1}{\mu} (\phi_p^b + \phi_\alpha + \sum \phi^k) \]  \[ \dot{U} = M(u) \text{ with } u = \frac{1}{\mu_{\alpha\beta}} \sum \phi_{\alpha\beta}. \]

in which \( M(u) \) is the rotation matrix generated from the moment vector \( u \). We effectively used \( 1/\mu_{\alpha\beta} = 0 \).

**1.4. Validations.** To validate our numerical method and its implementation, we first simulated a MT bundle confined inside an ellipse cell of tension \( \sigma \) and volume \( \frac{1}{2} \pi R_0^2 \). A classical result of analytical mechanics is that a filament should buckle under a tangential force \( f \) if this force is larger than a critical force:

\[ f^* = \frac{\kappa \pi^2}{L^2}. \]  

We confined the MT in a deformable ellipsoid, which thus takes the shape of a prolate ellipsoid. Let us call \( a_1 = R \) the longer axis of this ellipsoid, and the shorter axis \( a_2 \). \( a_3 = \sqrt{R^2/a_1} \). The force exerted on the MT is \( f_a = \frac{1}{2} \sigma \partial_\alpha S(R, \sqrt{R^2/a_1}, \sqrt{R^2/a_2}) \), with \( S \) defined in Eq. 7. Starting with a MT of length \( L \), buckling will occur for a critical tension:

\[ \sigma^* = \frac{2 \kappa \pi^2}{R^2} \left( \partial_\alpha S(R, \sqrt{R^2/a_1}, \sqrt{R^2/a_2}) \right)^{-1}. \]

In simulations, we find that the MT buckles for \( \sigma > \sigma^* \), as we predicted (Fig. S1).

**2. Mechanics of a Confined Elastic Ring**

**2.1. Formulation.** Let us consider a rod of length \( L \) lying on a sphere of radius \( R \). We can describe this rod by its position \( r \), parametrized by its arc length \( s \), such that the energy reads:

\[ E(R, L) = \frac{\kappa}{2} \int_0^L r^2 \; ds. \]

Because the rod lies on the unit sphere, and because \( s \) is the arclength, we have the constraints:

\[ \|r\|^2 \leq R^2 \quad \text{and} \quad \|s\|^2 = 1. \]

We can introduce this as constraints in the energy using two Lagrange multipliers \( \alpha \) and \( \beta \), to define:

\[ E = \frac{\kappa}{2} \int_0^L \left[ r^2 + \alpha (R^2 - \|r\|^2) + \beta (\|s\|^2 - 1) \right] \; ds. \]

Minimizing this energy yields the Euler-Lagrange equation:

\[ \ddot{r}(s) = \kappa(s) (r(s) \times \dot{r}(s)) - \frac{1}{R^2} \dot{r}(s), \]

where \( \gamma \) is a negative constant (35). Finally, one needs to find the value of \( \alpha \) and \( k_0 \), such that the curve is closed and of length \( L \):

\[ r(L) = r(0) \quad \text{and} \quad \dot{r}(L) = \dot{r}(0). \]

Numerically, we determined \( \gamma \) and \( k_0 \) using a shooting method.

**2.2. Case of a Weakly Deformed Ring.** For a weakly deformed ring, Eq. S22 can be simplified to

\[ \ddot{r} = \frac{\gamma}{R^2} \dot{r}. \]

Periodicity imposes \( \sqrt{-1} \gamma \rightarrow m \), when \( L \rightarrow 2\pi R \), in which \( m \in \mathbb{N} \). Because the lowest energy curve has a period \( L/2 \), we can conclude that \( m = 2 \), i.e., \( \gamma \rightarrow -4 \) for \( L \rightarrow 2\pi R \). Although analytically solving the full shape equation \( R(s) \) is arduous (18), even in this weakly deformed approximation, we can construct a shape equation that satisfies Eq. S24 for small deformation as follows:

\[ R = R \left( \frac{1 - b}{\sin t + b \sin 3t}{(1 - b) \cos t - b \sin 3t}{2\sqrt{(1 - b) \cos 2t}} \right), \]

in which \( 0 \leq t \leq 2\pi \) is an angle coordinate. For small deformations \( b \rightarrow 0 \), one finds:

\[ \ddot{r}(s) = 6 \sqrt{b} \cos 2s/R + O \left( b^2 \right) \]

\[ \ddot{r}(s) = \gamma \times 6 \sqrt{b} \cos 2s/R + O \left( b^2 \right). \]

with \( \gamma = -4 \) as expected. From Eq. S25, we can compute the bending energy of the MB:

\[ E(R, b) = \int_0^{2\pi} \left( \frac{1}{R^2} + k_f^2 \right) \|\dot{r}(s)\|^2 \; dt. \]

For small deformations \( b \rightarrow 0 \), we have:

\[ E(R, b) = \frac{\kappa}{2 R} (2\pi + 36 \pi b + O(b^2)). \]

We can also compute the length of the MB, and the energy:

\[ L(R, b) = 2\pi R (1 + 6b + O(b^2)). \]

\[ E(R, L) \rightarrow \frac{\kappa}{2 R} \left( 2\pi + 3\frac{L - 2\pi R}{R} \right). \]

We then find the force exerted by a nearly flat ring on the sphere \( L = 2\pi R \):

\[ f_b = \lim_{L \rightarrow 2\pi R} \partial_\beta E(R, L) = \frac{8\pi \kappa}{R^2}. \]

This result is in agreement with solving the full shape equation (Eq. S22), as illustrated in Fig. S2. \( f_b \) is the force exerted by a nearly flat ring on a sphere: by construction, it is also the critical force at which a ring will buckle. Numerically, we can study ring buckling in two cases: when the ring is undergoing an elastic confinement, and when the ring is confined by a deformable ellipsoid.

**2.3. Ring Under Elastic Confinement.** Let us consider a ring of length \( L \) confined in a sphere of radius \( R \), such that \( L = 2\pi (R + \epsilon) \) by an elastic confinement \( k \) (see ref. 29 for the implementation of confinement). The confinement force is here \( f_c = k_n \), in which \( n \) is the number of points describing the discrete ring. The ring will buckle if \( f_c > f_b \); using Eq. S32, we find that the ring will buckle above a critical confinement:

\[ k_c = \frac{8\pi \kappa}{\pi \epsilon R^2}, \]

in which \( n = L/s \), where \( s \) is the segmentation.

**2.4. Ring Confined in a Deformable Ellipsoid.** Using our computed value of \( f_b \), we can compute analytically the critical value of the tension that will buckle a ring in a deformable space, assuming...
that space to be ellipsoid and near-spherical. For this, we take the very same approach as we did for the bundle in a prolate ellipsoid, although now the ellipsoid is oblate, and the buckling force is that of a ring rather than an open bundle.

\[
\sigma^* = \frac{f_{BB}}{\partial R S(R, R, R^3/2^3)}.
\]  

[S34]

3. Simulation Parameters

The parameters used for Figs. 4 and 5 were:

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Ring rigidity</td>
<td>( \kappa_r )</td>
<td>1 pN ( \mu )m^2</td>
</tr>
<tr>
<td>Time step</td>
<td>( dt )</td>
<td>2 ( \times 10^{-3} ) s</td>
</tr>
<tr>
<td>Filament segmentation</td>
<td>( ds )</td>
<td>3 ( \times 10^{-2} ) ( \mu )m</td>
</tr>
</tbody>
</table>

For the incompressible elastic ring in a fixed shape ellipsoid (Fig. 4), we built a closed ring by linking the first and last point of the filament with a zero-resting length link of rigidity \( \kappa_c = 10^3 \) pN/\( \mu \)m. We also add a torque component (29) to ensure that the bending elasticity is uniform in every point of the ring. In these simulations, additional parameters were:

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Cell major radius</td>
<td>( R )</td>
<td>1 ( \mu )m</td>
</tr>
<tr>
<td>Cell minor radius (thickness)</td>
<td>( r )</td>
<td>0.24 to 1 ( \mu )m</td>
</tr>
<tr>
<td>MB length</td>
<td>( L )</td>
<td>6.5 ( \times 1.0345 \times 2\pi ) ( \mu )m</td>
</tr>
<tr>
<td>Confinement stiffness</td>
<td>( k )</td>
<td>1 to 40 pN/( \mu )m</td>
</tr>
<tr>
<td>Thermal energy</td>
<td>( k_BT )</td>
<td>10^{-6} pN/( \mu )m</td>
</tr>
</tbody>
</table>

4. Experimental Methods

The experiments were performed on platelets extracted from the blood of the common inbred laboratory mouse strain (C57BL/6) and prepared according to standard protocols (44). Blood was collected by cardiac puncture and mixed with 200 \( \mu \)L of acid–citrate–dextrose solution to prevent coagulation. Once obtained, the blood was immediately centrifuged for 4 min at 200 \( \times \) g. The upper phase (platelet-rich Plasma), was carefully removed and centrifuged at 2,000 \( \times \) g for 2 min. The plasma was discarded, and the platelet pellet was resuspended in Tyrode’s albumin buffer. We labeled MTs with 50 nM SiR tubulin (Spirochrome) and incubated the cells for at least 1 h before imaging. Imaging was performed by using a spinning disk microscopy setup (Perkin-Elmer Ultraview VoX). Live platelets were imaged by using a 63\( \times \) (1.4-NA) oil objective, which produced images with a lateral pixel size of 104 nm. The 3D stacks were acquired with a spacing of 0.4 \( \mu \)m in the axial dimension. An image stack was acquired every 5 s over 10 min. The image analysis was performed by using Fiji (fiji.sc/Fiji).

For the simulations of the incompressible elastic ring in a deformable ellipsoid (Fig. 5), we used:

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Cell volume</td>
<td>( V )</td>
<td>4( \pi/3 ) ( \mu )m^3</td>
</tr>
<tr>
<td>MB Length</td>
<td>( L )</td>
<td>(1 to 1.6) ( \times 2\pi ) ( \mu )m</td>
</tr>
<tr>
<td>Cortical tension</td>
<td>( \sigma )</td>
<td>10^{-2} to 17 pN/( \mu )m</td>
</tr>
<tr>
<td>Ellipse effective viscosity</td>
<td>( \mu )</td>
<td>340 ( \mu )m pN^{-1}s^{-1}</td>
</tr>
<tr>
<td>Confinement stiffness</td>
<td>( k )</td>
<td>200 pN/( \mu )m</td>
</tr>
<tr>
<td>Thermal energy</td>
<td>( k_BT )</td>
<td>10^{-5} pN/( \mu )m</td>
</tr>
</tbody>
</table>

Tolerance parameter for cell volume \( \epsilon \) | 10^{-4} |

Fig. S1. Phase diagram of the degree of buckling as a function of the length and the tension. Red means that the filament is buckled and gray that it is flat. The dashed line represents the critical tension calculated in Eq. S16.
Fig. S2. Bending energy of an incompressible elastic ring of length $2\pi R_0$ (the MB) in a sphere of radius $R < R_0$. The solid line represents the numerical solution to the Euler–Lagrange equations (Eq. S22), while the dashed line represents the small deformation approximation, Eq. S32.

Other Supporting Information Files

Dataset S1 (TXT)